



SEMINAR

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SOME PLEASANT SURPRISES ABOUT THE PERFORMANCE OF RECYCLED CONSTRUCTION MATERIALS

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Aged Material Properties of Cold In-Place Recycled Asphalt Roads

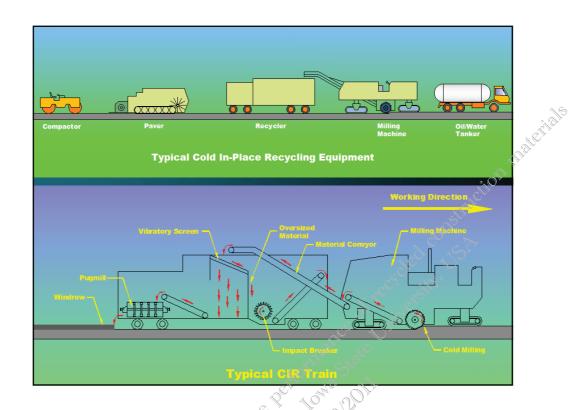
Sponsor: Iowa Highway Research Board

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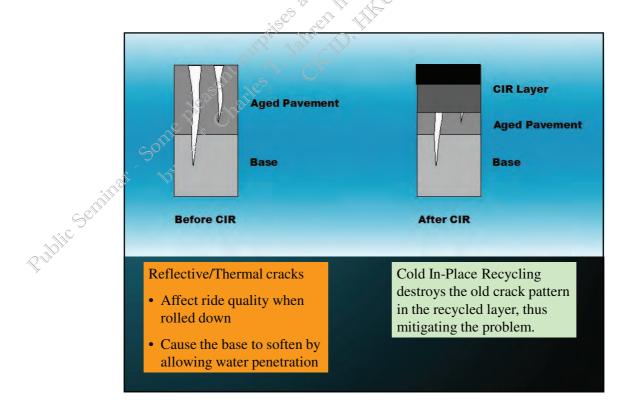
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Problem Statement

- Recycled roads have inconsistent performance
- Prominent factors:
- Support conditions

 Aged engineering properties of the CIR materials

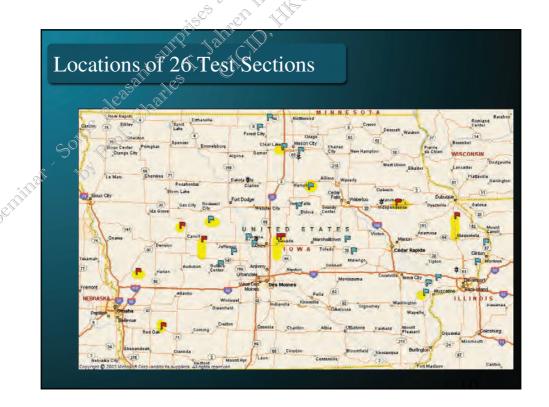
 Aged Helder of the CIR materials

Objectives

- o answer two questions:
 - How do aged engineering properties of CIR materials, traffic and subgrade conditions affect the pavement performance?
 - What changes should be made with regard to design, material selection and construction in order to improve the performance of future recycled roads?

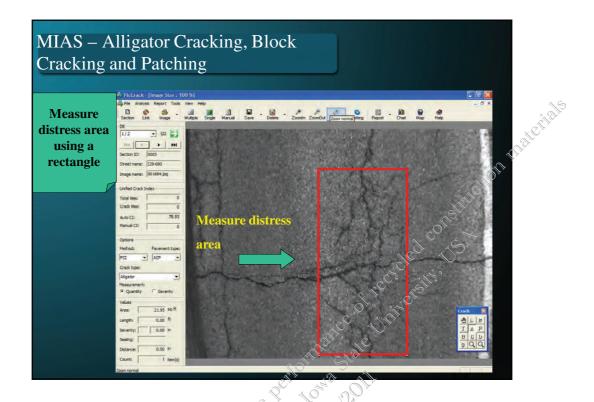
Selection of CIR Test Sections

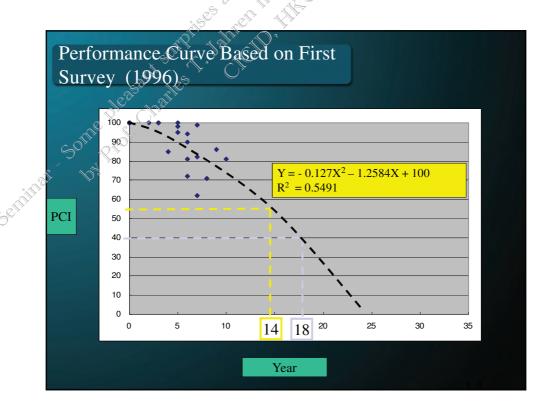
- Eighteen 1,500-ft old test sections, which were surveyed in 1996 and 1997, were selected for re-evaluation in 2005.
- Eight 1,500-ft new test sections were surveyed in 2005.
- Test sections were categorized by:
 - Age
 - Traffic level
 - Subgrade support level

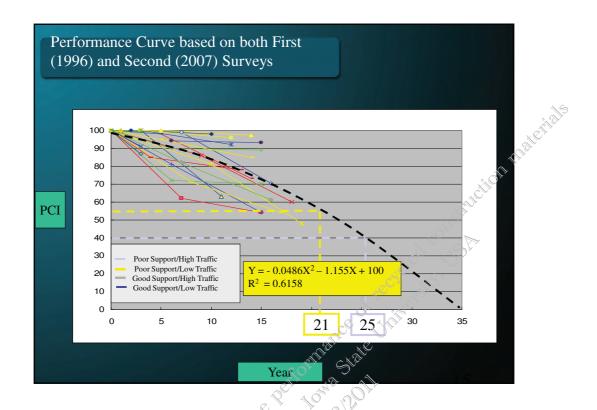


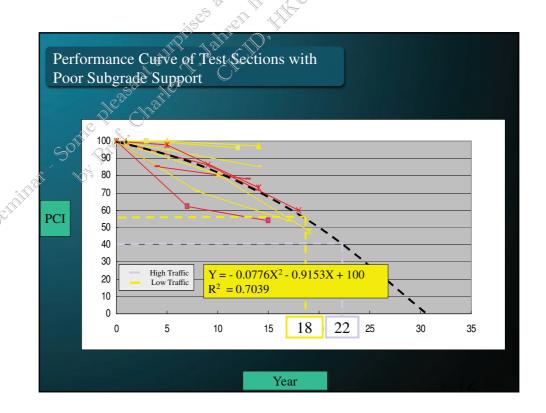
	CIR Pro		npling Matrix	Poor S	Support
		(>Subgrade Mo	dulus of 5,000 psi)	(< Subgrade Mod	lulus of 5,000 psi)
		Low Traffic (0~800)	High Traffic (>800)	Low Traffic (0~800)	High Traffic (>800)
	Young (1999~)	IA-44, Harrison	US-20, Delaware US-61, Jackson IA-48, Montgomery	N-58, Carroll N. of Breda, Carroll S-14, Story	S-27, Story
A g e	Medium (1992~ 1998)	-	IA-175, Calhoun IA-4, Guthrie F-70, Muscatine	V-18, Tama E-52, Boone T-16, Butler	G-28, Muscatine D-35, Hardin
	Old (1986~ 1991)	R-34, Winnebago B-43, Cerro Gordo R-60, Winnebago	S.S.L., Cerro Gordo Z-30, Clinton E-66, Tama	198th St., Boone E-50,Clinton	Y-14, Muscatine IA-144, Greene

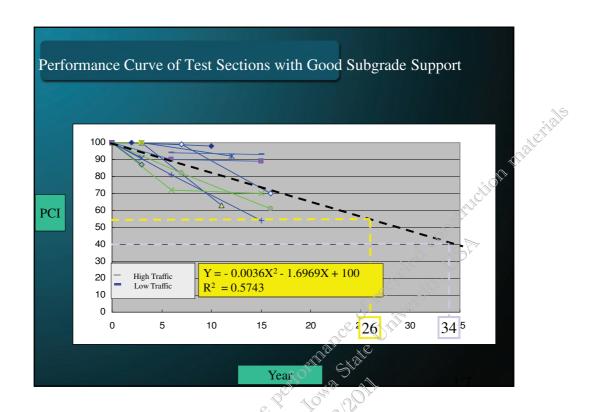


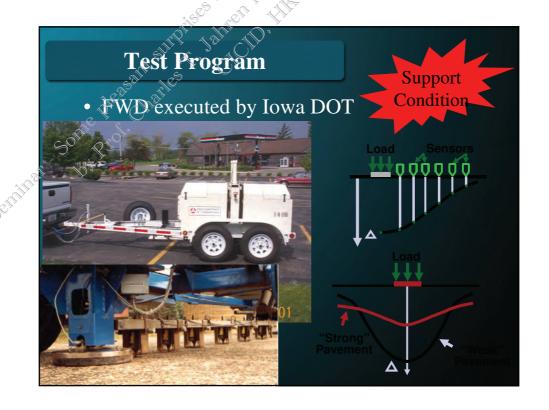




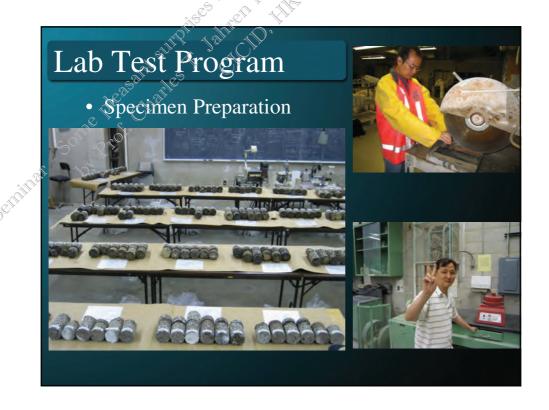


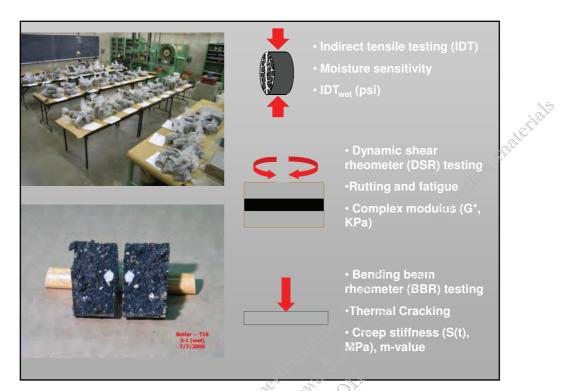






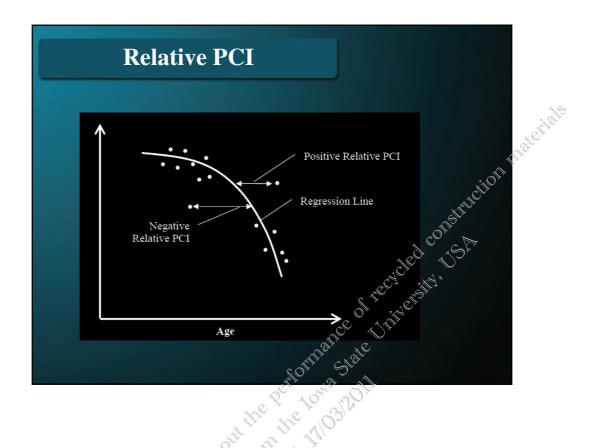


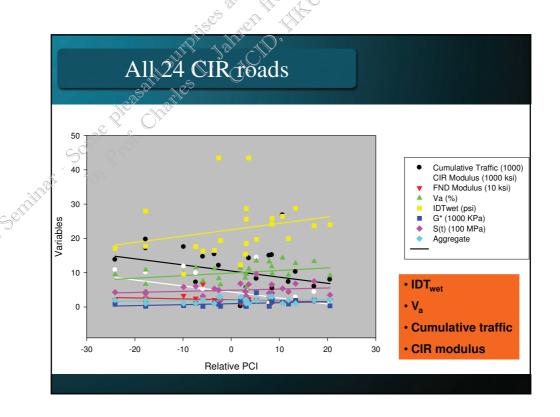




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	Type of Property	Property	Typical HMA	CIR in this study	
Mic Seriire	Mix	V _a (field measured, %)	5 ~ 9	4.5 ~ 14.3	
	Binder	G*/sin(delta)	> 2.2	230 ~ 4,700	
CEITH.	Binder	G*sin(delta)	< 5,000	170 ~ 3,600	
13C	Binder	Penetration (dmm)	20 ~ 30	0 ~ 30.3	
30 pr	Binder	S(t) (Mpa)	< 300	204 ~ 962	
	Binder	m-value	> 0.3	0.16 ~ 0.32	
	Pavement Layer Structural	Pavement modulus (ksi)*	100 ~ 6,000	200 ~ 4,400	
	Subgrade Layer Structural	Subgrade modulus (ksi)*	1 ~15#	3 ~ 16 [@]	





Results - all CIR roads

- $R^2=0.5937$
- $R^2_{adi} = 0.5357$

Term	Estimate	P-value	Significance at 0.05 level?
$(V_a)^2$	2.45	0.0021	Yes
CIR modulus	-1.38	0.0027	Yes
(Cumulative Traffic) ²	-0.00026	0.015	Yes
			rec, religi

- * V_a is air void (%)
- * Air voids are voids between the aggregate particles in the compacted CIR layer that are filled with air

Es apor Prouting

Results Vlow traffic roads

- $^{\bullet}$ R²=0.5213
- $\Re^2 = 0.4256$

Term	Estimate	P-value	Significance at 0.05 level ?
IDT _{wet}	0.361	0.008	Yes
(CIR modulus) ²	-1.28E-06	0.0845	No

Results - high traffic roads

- $R^2=0.5213$
- $R^2_{adi} = 0.4256$

Term	Estimate	P-value	Significance at 0.05 level ?
CIR modulus	-1.50E-03	0.0015	Yes
(G*) ²	3.98	0.0914	No.C
			St. Act

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Conclusions

- Predicted service life 21 to 25 years
 - Longer w/ good support (up to 34 yr)
 - Shorter w/ poor support (as little as 18 yr)
 Support more important than traffic
 - within range of analysis (< 2K AADT)</p>
 - Traffic has little effect on roads w/ good support
- Longitudinal and alligator cracking increased... not transverse cracking
 - Rutting, patching and edge cracking associated with poor support

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Conclusions

Better performance is associated with:

- V_a (air voids) is higher
- Range: 6 to 12%
- CIR modulus is lower (more elastic)
- Range: 200 to 4,400 ksi
 - -- within the range of the analysis

Poor Performance will result from higher V_a and lower CIR Modulus

HMM Stress-relieving layer

Conclusions

- Within the range of the data analyzed, higher value of IDT_{wet} significantly and positively affected pavement performance of low traffic roads
- As would be expected, roads with higher cumulative traffic exhibited more distress

Performance Evaluation of Concrete Pavement Granular Subbase — Pavement Surface Condition Evaluation

Sponsored by

Iowa Highway Research Board IHRB Project TR-554

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IOWA STATE UNIVERSITY

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- Many people assisted the authors in identifying and locating projects for testing, controlling traffic, and refining research tasks.
- Reilly Construction is gratefully acknowledged for brainstorming the test locations of several old RPCC projects during a winter meeting.
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- Mike Heitzman, Chuck Lee and Kelly Popp with Iowa DOT and Kevin McLaughlin (Iowa State University Undergraduate Student) assisted with the electronic document search
- Field team, including Heath Gieselman, Bryan Zimmerman, Bob Steffes, and Jeremy McIntyre with Iowa State University.
- John Vu allowed the authors to use the lowa Department of Transportation field permeameter.

Introduction (continued)

What are the concerns of using RPCC for pavements?

- Recycled PCC aggregate reduces permeability, clog the drainage systems.
- High pH leachate corrodes metal drainage pipes, damages vegetation.
- Question on the stability of subbase layer using recycled PCC.

Literature Review - RPCC

- Experience breakage of particles, increase fines
- Reduce the freeze-thaw resistance and permeability
- High % fines & low permeability > pore water pressures develops under the pavement that reduce shear strength of base and subgrade layers
- High pore water pressures > cracks on pavement due to bulging of pavement and failure on the pavement surface under traffic load
- Cement hydration of the recycled PCC can reduce void ratio

Research Objectives

- Determine if RPCC pavement subbase is performing adequately.
- Evaluate subbase stiffness and permeability by performing multiple tests within a given test section using semi non-destructive methods.
- Determine the gradation of the subbase materials.
- Conduct crack and performance survey of pavement.
- Summarize projects used RPCC for pavement construction in Iowa.

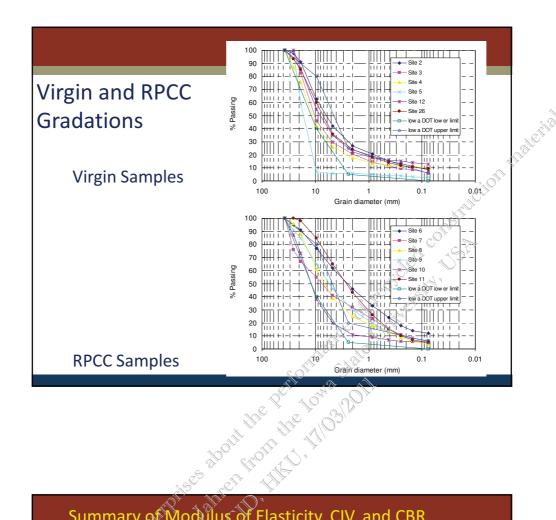
Research Plan

- Visit 26 locations: 21 recycled and 5 virgin material sites
- At each site, conduct: LWD, Clegg hammer, DCP, permeability, sampling, and pavement crack survey.
- Compare and correlate performance of recycled PCC with virgin materials.
- Develop guidelines and specifications for pavement design using recycled PCC aggregate materials



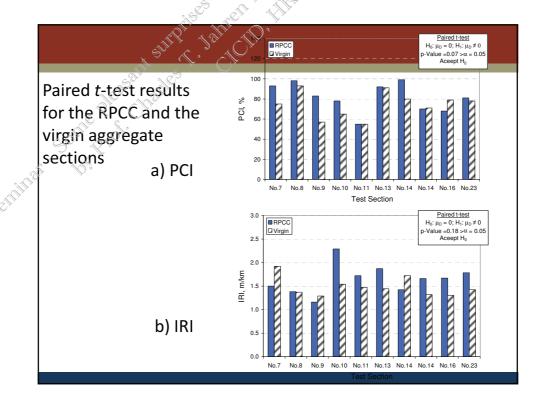


	New State Control of the State		
	Property Solvers	Natural aggregate	Recycled concrete aggregate
	Specific Gravity	2.4 - 2.6	2.2 - 2.3
hlic Seltitre	Estimated loss based on the modified Micro-Deval test (%) (*)	11 - 32	16 - 65
	USGS	GP-GM	Variable



	Summar	y of Mod	ulus of E	Elasticit	y, CIV, and	CBR	
		E _{IWD} (I	Mpa)		Subbase		
		Subbase	Subgrade	CIV	CBRa	CBRb	_
	Max value	2126	150	638	100*	100*	_
	Min Value	43	33	17	21.5	18	
	Average	535.3	66.1	89.4	73.0	66.9	
	STDEV	553.5	39.3	119.4	27.1	28.4	
	COV (%)	103.4	59.5 Ited from CIV v	133.6	37.0	42.5	
zojblic Seltilite	Estimate	*: converted	nted from PI va value is higher posite v a	than 100 alues fr	om LWD		
>				Subbas			
			measuremen		Composite me	-	
	N 4 l	Stress, kP			MPa/m	pci	
	Max value		186	659	21093	77706	
	Min value		117	16	329	1210	
	Avg	2	162	142	4991	18386	
	STDEV COV (%)		29 11	156 110	5359 107	19744 107	
	COV (%)		11	110	107	107	

	1.	ı.	
Subbase material	<u>k_{1 (5 cm)}</u> (ft/day)	K _{2 (10}	cm)
Max values	(It/uay)	(ft/d	
		8.1	19.09
Min values		0.01	0.01
Average		2.73	6.39
STDEV		4.65	11.00
COV (%)	1	70.7	172.1
Permeability of	RPCC Materi	als	11.00 172.1
Permeability of			~ CO,
·	RPCC Materi k _{1 (5 cm)} (ft/day)	als k _{2 (10} (ft/d)	cmA & A
Permeability of Subbase material Max values	<u>k_{1 (5 cm)}</u> (ft/day)	k _{2 (10}	cmA & A
Subbase material	k _{1 (5 cm)} (ft/day)	k _{2 (10} (ft/d	cmA & A
Subbase material Max values Min values	<u>k_{1 (5 cm)}</u> (ft/day)	k _{2 (10} (ft/d) 3.31 0.02	cm) 5.14
Subbase material Max values	k _{1.(5 cm)} (ft/day)	k _{2 (10} (ft/d	5.14 0



Summary of Findings -- Lab and Field

- Modulus of elasticity of RPCC subbase materials is high and variable from one project to another.
- CIV obtained from Clegg hammer tests are high.
- RPCC subbase layers normally have low permeability.

Summary of Findings -- Distress Survey

- The current pavement surface condition of RPCC subbase sections is comparable to that of virgin aggregate subbase sections in terms of the Pavement Condition Index (PCI) and the International Roughness Index (IRI).
- Based on the evaluation of representative RPCC subbase pavement sections with comparisons to virgin aggregate subbase sections, it can be concluded that the RPCC pavement subbase is performing adequately.

General Conclusions

- Recycled materials behave differently from non-recycled materials.
- In some cases these behaviors seem to render the recycled materials as inferior to their non recycled counterparts
 - CIR has higher voids % and less stiffness in comparison to non recycled hot mix asphalt.
 - RPCC has less permeability in comparison to crushed rock

General Conclusions

- Recycled material properties may provide advantages.
 - Lower stiffness and higher air voids in CIR apparently mitigate crack reflection
 - Higher stiffness in RPCC layer may increase structural effectiveness and make up for lack of permeability.

Recommendations

- Investigate properties of recycled materials fully and on their own merits
 - Avoid considering them to be inferior versions on non recycled materials.
- Consider including recycle materials in a way that takes advantage of their desirable characteristics.
 - Crack mitigation layer for asphalt overlay projects from CIR
 - Strengthen pavement base with RPCCin a manner similar to that of asphalt or cement treated base.

